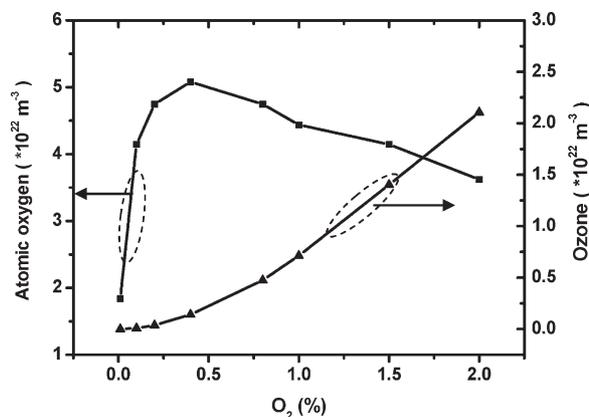


A Global Model for the Identification of the Dominant Reactions for Atomic Oxygen in He/O₂ Atmospheric-Pressure Plasmas

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Atmospheric pressure plasmas have attracted great interests and been widely used in biomedical applications such as sterilization, coagulation, wound healing, and cancer cells treatment. The reactive oxygen species (ROS) generated in atmospheric pressure plasmas have been believed to play a crucial role in these biomedical applications. The experimental measurement of the atomic oxygen density showed that the highest density was measured at an admixture of 0.5% of O₂. The similar trend of the atomic oxygen density varying the concentration of O₂ was reproduced through a global model of He/O₂ in atmospheric pressure plasmas. The evolution of the dominant production and loss reactions for the atomic oxygen was analyzed. With increase in the concentration of O₂, the atomic oxygen was produced mainly by the dissociation of O₂ and lost through the recombinations with themselves and oxygen molecules.



Introduction

Atmospheric pressure plasmas have been widely used in biomedical applications such as sterilization,^[1] coagulation,^[2] wound healing,^[3] and inducing apoptosis of cancer cells^[4] due to their great reactivity, low temperature property, and no needs for the expensive and complex vacuum system. Various kinds of atmospheric pressure plasmas such as the atmospheric pressure plasma jet, the dielectric barrier discharges, and the needle plasma have

been developed and their generation has been achieved over a wide spectrum from dc, through kilohertz and megahertz to microwave.^[5–8] However, a quantitative diagnostic of atmospheric pressure plasmas is quite challenging due to their often small dimension, short duration, and the limited applicability of conventional low pressure diagnostic techniques. As a result, a computer simulation is a powerful tool that can complement experimental observations and help in unraveling the physics underpinning these discharges.

Admixtures of He and O₂ are often used in atmospheric pressure plasmas because of their satisfactory compromise between plasma stability and chemical reactivity.^[9,10] The reactive oxygen species (ROS) are believed to play a crucial role in these biomedical applications.^[1,9] The chemistry of these discharges is therefore of great interest and understanding the main reactions involved in the generation of reactive species is a first step needed in order

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to optimize the plasmas. To that end, we have developed a global model^[11,12] for He/O₂ discharges. The model incorporates a total of 98 reactions, something that cannot be handled by today's particle-in-cell Monte Carlo collision simulations and that slows down significantly fluid models. Although this model is not able to capture spatial variations often observed in actual discharges, it is a powerful tool for identifying main species and reactions from a large set of chemical processes.

Model

The global model was widely adopted as a tool to understand the characteristics of the low-pressure capacitively-coupled discharges,^[11,13] the hollow cathode,^[14] and the atmospheric pressure glow discharge.^[12] Its fast computational time and the capability of the easy implementation for taking into account a number of species and reactions are the great advantages of this model to be chosen.

In the model of He/O₂ atmospheric pressure plasmas, 15 species, namely, electrons *e*, helium ions He⁺, excited helium atoms He*, dimer helium ions He₂⁺, excited dimer He₂^{*}, positive oxygen molecule ions O₂⁺, negative oxygen molecule ions O₂⁻ and O₃⁻, excited oxygen molecules O₂(¹Δ_g) and O₂(¹Σ_g⁺), ozone O₃, ground-state atomic oxygen O(³P), positive atomic oxygen ions O⁺, negative atomic oxygen ions O⁻, excited oxygen atoms O(¹D) are considered. Our model of He/O₂ includes 98 reactions for He/O₂ mixture selected from publications on discharge modeling in the literatures.^[11,15–23]

The model describes a plasma source of volume *V* and its surface area *S*. The plasma is assumed to be nearly spatially uniform and the power is absorbed uniformly into the plasma. In an arbitrary volume (*V*) enclosed by the surface area (*S*), the time-dependent particle balance equations for each species density (*n_k*) are taken to be

$$\frac{d}{dt}(n_k) = (s_k - l_k) - \left(\frac{S}{V}\right)\Gamma_k \quad (1)$$

that describes the balance between source and loss to result from the reactions among species and the wall loss due to the thermal diffusion, where *n_k* is the density of species, *s_k* and *l_k* are the generation and loss rate due to the chemical reactions, respectively, and Γ_k is the flux into the boundary. Assuming the ions and radicals are Maxwellian distributions with the room temperature, the flux at the boundary is defined as

$$\Gamma_k = \frac{1}{4} n_k \bar{v}_k \quad (2)$$

where \bar{v}_k is the averaged velocity of species. For the quasi-neutrality, the flux into the boundary of the electrons is defined as

$$\Gamma_e = \sum_i \Gamma_{+,i} - \sum_j \Gamma_{-,j} \quad (3)$$

where Γ_{\pm} is a positive or negative ion flux at the boundary.

The power balance equation to consider the balance between the input absorption power and the power loss of electrons by the collisions with other species is taken to be

$$\frac{d}{dt} \left(\frac{3}{2} n_e T_e \right) = P_{\text{abs}} - P_e \quad (4)$$

where *T_e* is the electron temperature in eV, *P_{abs}* the input power density, and *P_e* is the power loss of electrons due to the chemical reactions. Electrons are assumed to have a Maxwellian energy distribution function. Equation (1) for each species and Equation (4) were solved simultaneously to calculate the each species density and the electron

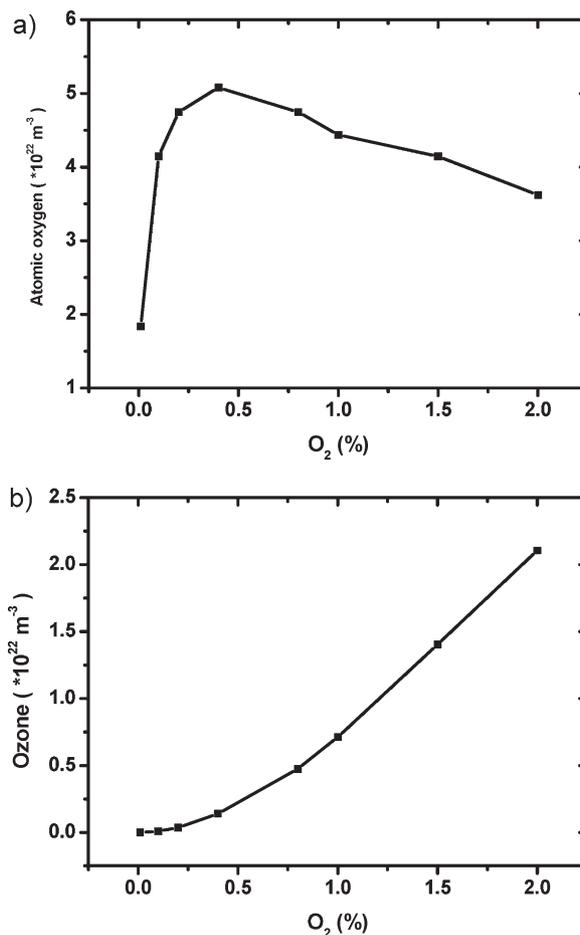
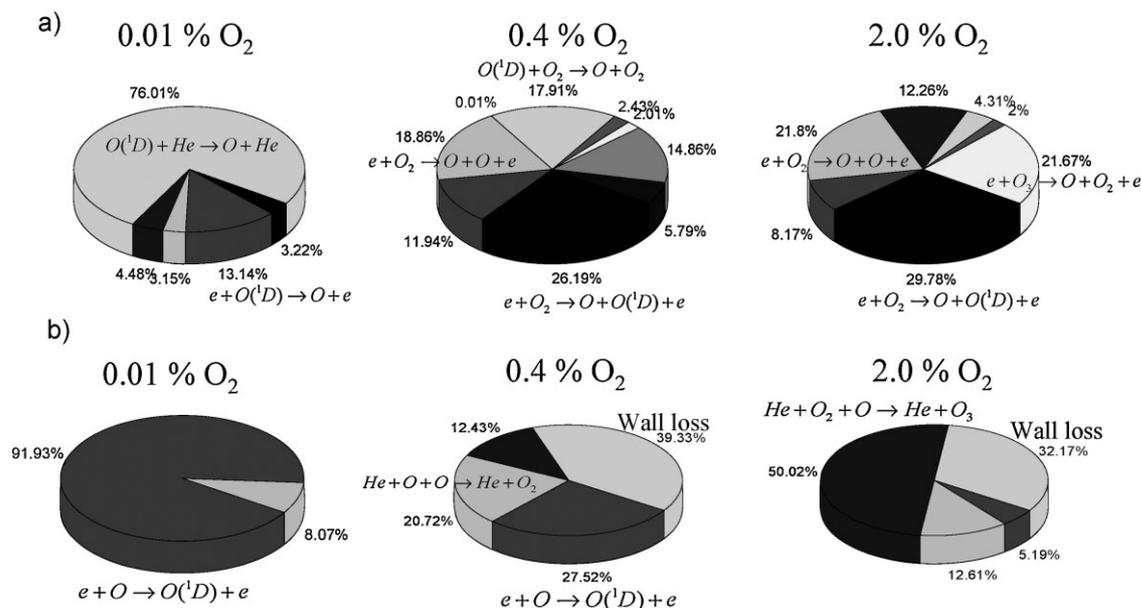


Figure 1. (a) The atomic oxygen and (b) the ozone density for various concentration of O₂ (absorbed power = 330 W · cm⁻³).



■ Figure 2. Diagrams for proportions of the atomic oxygen (a) production and (b) loss reactions concentrations of O₂, 0.01, 0.4, and 2.0%.

temperature. The densities of neutral species of helium and oxygen molecules were fixed at the initial values given by the fraction of an admixture at the atmospheric pressure. The gas temperature was fixed at room temperature, 300 K since the atmospheric pressure plasmas for biomedical applications are non-thermal discharges and their gas temperature is not far from the room temperature. For the simplicity, the gas heating due to the collisions among feeding gases and other species was not considered.

Results and Discussion

Figure 1(a) and (b) show the atomic oxygen and ozone densities in He/O₂ atmospheric pressure discharges while varying the concentration of O₂ with the input power of 330 W · cm⁻³, which is the power absorbed when the input power of 10 W applied to the plasma volume of 30 mm³ and is close to the magnitude used in ref.^[6] It is believed that those species are crucial agents to deactivate bacteria and cause disinfections or sterilizations.^[1,9] Knake et al.^[6] measured the atomic oxygen density in the discharge core while changing the concentration of O₂ and showed the highest oxygen production at an admixture of 0.5% of O₂. As shown in Figure 1(a), the similar trend is observed through the global model and the maximum atomic oxygen production appears at 0.4% of O₂. However, the ozone density does not show a maximum value at a certain

admixture of O₂ up to 2.0% and keeps growing with increase in the concentration of O₂.

The evolution of the atomic oxygen density with the concentration of O₂ is analyzed in terms of the dominant production and loss reactions for the atomic oxygen. The diagrams in Figure 2(a) and (b) show the proportion of each production and loss reaction rate for the atomic oxygen with respect to the total reaction rates. At the low concentration of O₂ (0.01%), most of atomic oxygen are generated through the de-excitation processes of O(¹D) by colliding with electrons and neutral helium atoms, as shown in Figure 2(a). With increase in the concentration to 0.4% of O₂, the atomic oxygen is produced through the dissociation processes of oxygen molecules by electrons and partly, the de-excitation of O(¹D) by collisions with oxygen molecules. At the high concentration of O₂, the dissociations of O₂ and O₃ are the dominant processes to produce the atomic oxygen. Figure 2(b) shows the proportion of the dominant loss reactions for the atomic oxygen. At the low concentration (0.01%) of O₂, the atomic oxygen more than 90% are lost through the excitation process to O(¹D) by collisions with electrons. At the concentration of O₂ where the atomic oxygen density is maximum (0.4%), the portion of the excitation process of the atomic oxygen to O(¹D) is reduced and the thermal wall losses are the most dominant process and the recombination between the atomic oxygens is significant. At the high concentration of O₂ (2.0%), the recombination of the atomic oxygen and oxygen molecules by three body collisions with helium atoms are the most dominant loss process for the atomic

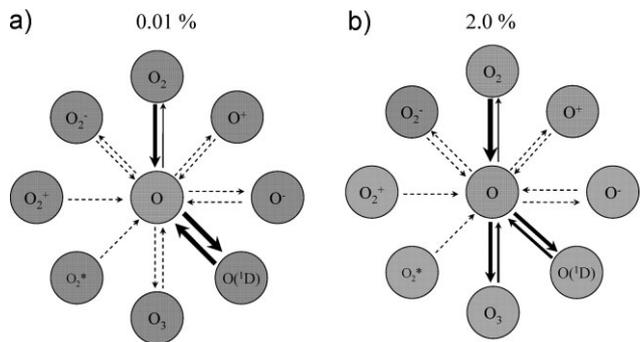


Figure 3. Diagrams for the relation between the atomic oxygen and other oxygen species for 0.01 and 2.0% of O_2 .

oxygen, and since those recombination processes produce the ozone, its density grows with increase in the concentration of O_2 .

Figure 3 shows the relations of the atomic oxygen with other oxygen species such as the excited oxygen and ionized oxygen molecules, and the width of the arrows indicates the relative magnitude of the reaction rate. At the low concentration of O_2 (0.01%), the atomic oxygen is excited by electrons into $O(^1D)$ and the $O(^1D)$ is de-excited into the ground state oxygen colliding with the electrons and oxygen molecules. At the high concentration of O_2 (2.0%), the atomic oxygen is generated by the dissociation of oxygen molecules rather than the de-excitation of $O(^1D)$ and is lost by the recombination with the oxygen molecules producing the ozone.

In the steady state, the total production and loss rates for a species have to be equal and its density remains constant as a result of a balance between them. Figure 4(a) shows the sum of all production (or loss) reaction rates for the atomic oxygen. Although the atomic oxygen density increases with increase in the concentration of O_2 to 0.4%, the total reaction rate is reduced. This results from the decrease in the electron density while increasing the concentration of O_2 since the oxygen molecule is the electro-negative gas. Figure 4(b) shows the total rates of reactions to produce the atomic oxygen through the dissociation of oxygen molecules and its proportion to total production rate. While the concentration of O_2 increases, the dissociation of oxygen molecules increases and the dissociation processes become significant to produce the atomic oxygen. The atomic oxygen can be lost through the electron-dominated loss reactions such as excitation, ionization, and attachment to change the atomic oxygen to $O(^1D)$, O^+ , and O^- . Figure 4(c) compares the proportions of the electron-dominated loss reactions rate and the dissociative productions rate to total reaction rate. It is noted that the reduction rate of the electron-dominated losses is larger than the increase rate of the dissociative productions with increase in the concentration of O_2 to 0.4%. Therefore, it is likely that the increase

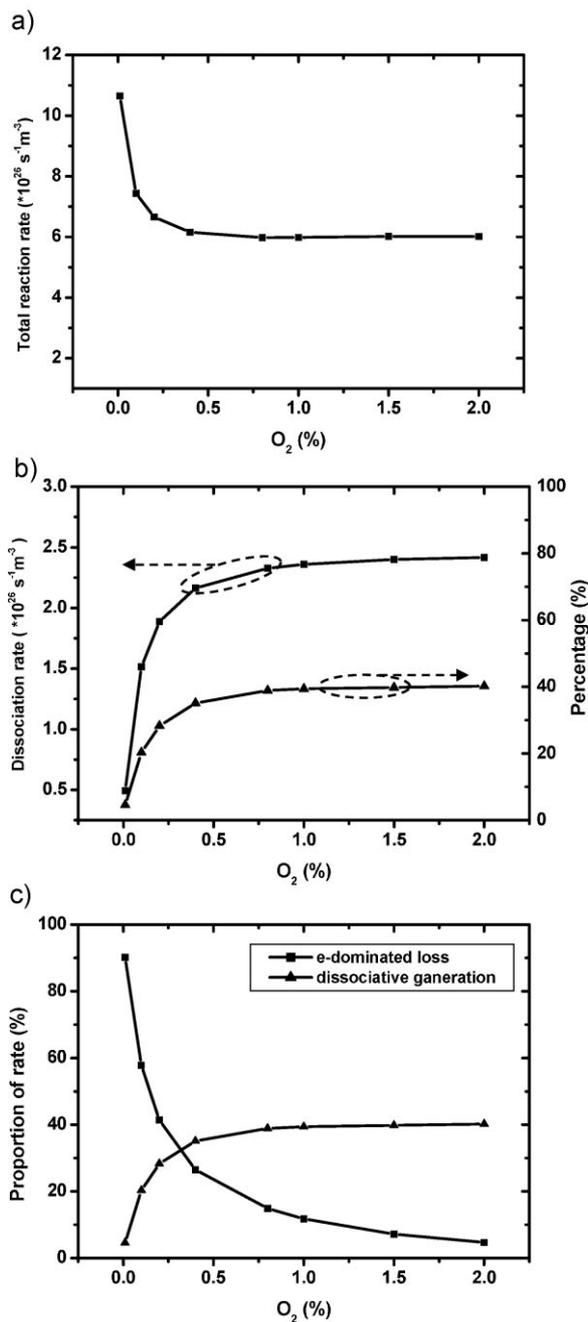


Figure 4. (a) The total reaction rate and (b) the dissociative production rate for the atomic oxygen and its proportion with respect to total production rate and (c) the comparison of the proportions of the electron-dominated loss and the dissociative generation for the atomic oxygen for various admixtures of O_2 .

in the atomic oxygen density at the low concentrations of O_2 (<0.4%) is attributed to the decrease in the electron-dominated loss reactions rate rather than the increase in the dissociative productions.

Figure 5 shows the evolution of the proportions of the dominant groups of the atomic oxygen loss processes such

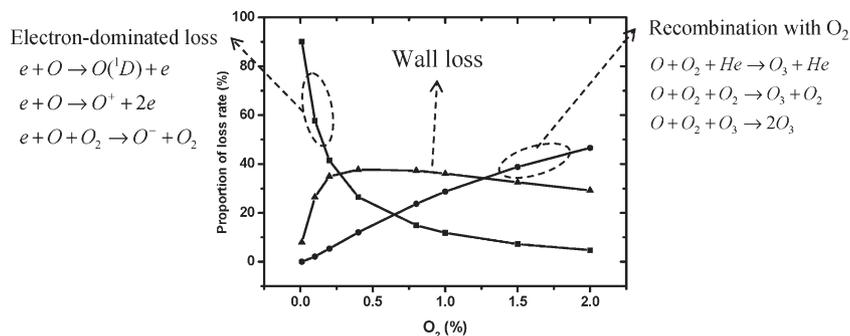


Figure 5. The loss rates of the electron-dominated loss, the wall loss, and the recombination loss with O_2 concentrations of O_2 .

as the electron-dominated losses, thermal wall loss, and recombination losses with oxygen molecules while varying the concentration of O_2 . At the low concentration of O_2 less than 0.3%, the electron-dominated loss reactions are the most dominant in the loss groups and are reduced with increase in the admixture of O_2 due to the decrease in the electron density. At the intermediate concentration (<1.0%), the wall loss dominates because the wall loss is proportional to the density and the atomic oxygen density increases with increase in the concentration of O_2 , as shown in Figure 1(a). At the high concentration of O_2 (>1.0%), since the population of oxygen molecules increases, the recombinations of the atomic oxygen with oxygen molecules are the most dominant processes and the ozone is produced as a byproduct. This evolution of the dominant loss reactions seems to be closely related with the density profile of the atomic oxygen as varying the concentration of O_2 .

Figure 6 shows the atomic oxygen densities for different input powers while varying the concentration of O_2 and they are normalized by a maximum value for each case to compare each other. With decrease in the input power, the

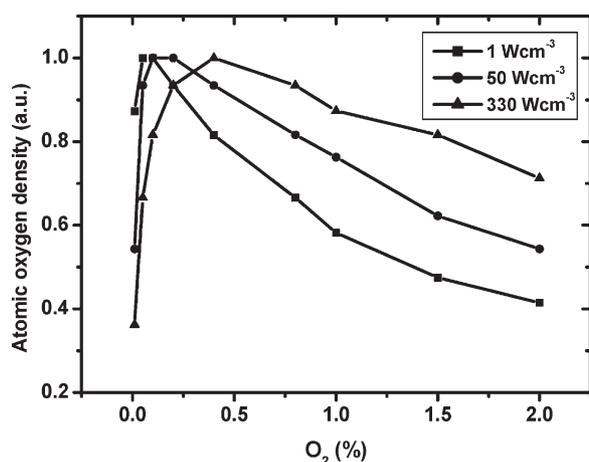


Figure 6. The atomic oxygen density normalized by the maximum density for different input power of 1, 50, and $330 \text{ W} \cdot \text{cm}^{-3}$ concentrations of O_2 .

concentration of O_2 to show a maximum density moves to lower value. The reduction of the relative atomic oxygen density with increase in the admixture of O_2 is faster at the case of the lower input power, as shown in Figure 6. The evolution of the dominant loss processes for the atomic oxygen is analyzed with change in the input power. With increase in the power absorbed at the admixture of 0.4% O_2 , the proportion of the recombinations with oxygen molecules and the wall loss are reduced and the electron-dominated

losses are increased, as shown in Figure 7(a). For the case of 0.05% of O_2 , the transition of the dominant loss process from the wall loss to the electron-dominated loss is observed while increasing the input power, as shown in Figure 7(b).

The global model is able to consider lots of reactions due to its fast computation time. If the model can select the

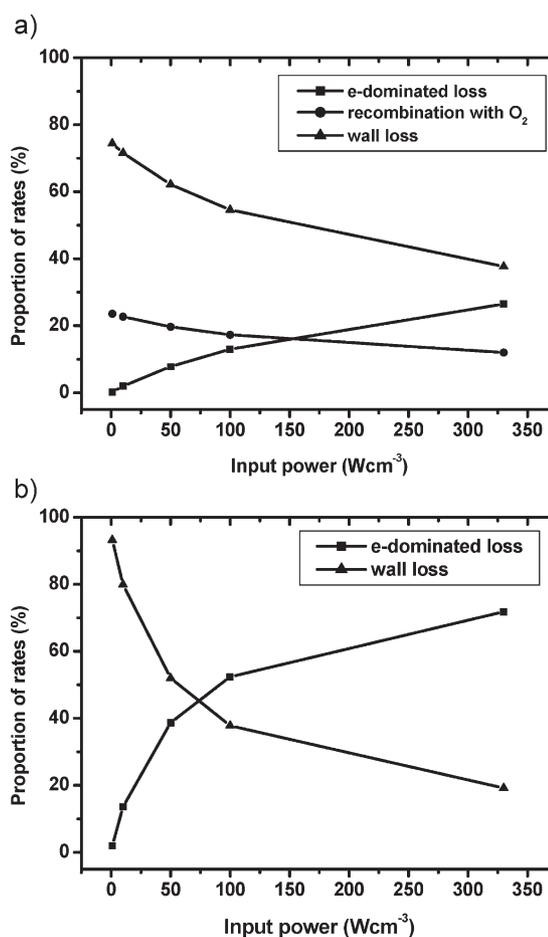


Figure 7. The proportions of different groups of loss processes for the atomic oxygen at (a) 0.4% and (b) 0.05% of O_2 .

Table 1. A list of key reactions for He/O₂ mixture. (*T_e* in volts and *T* in kelvins.)

No.	Reaction	Rate constant $\text{cm}^3 \cdot \text{s}^{-1}$	No.	Reaction	Rate constant $\text{cm}^3 \cdot \text{s}^{-1}$
R1 ^{a)}	$\text{O}_2^+ + \text{e} \rightarrow 2\text{O}$	4.8E-7	R19 ^{f)}	$\text{He}^+ + \text{O}_2 \rightarrow \text{He} + \text{O}_2^+ + \text{e}$	2.4E-10
R2 ^{a)}	$\text{e} + \text{O}_2 \rightarrow \text{O}^- + \text{O}$	8.8E-11	R20 ^{g)k)}	$\text{He} + \text{O}_2 + \text{O} \rightarrow \text{He} + \text{O}_3$	6.27E-34
R3 ^{a)}	$\text{e} + \text{O}_2 \rightarrow \text{O}_2^+ + 2\text{e}$	$9.0\text{E}-10T_e$ $\exp(-4.4/T_e)$	R21 ^{h)}	$\text{e} + \text{He} \rightarrow \text{He}^+ + \text{e}$	$2.3\text{E}-10T_e^{0.31}$ $\exp(-19.8/T_e)$
R4 ^{a)}	$\text{O}^- + \text{O} \rightarrow \text{O}_2 + \text{e}$	2.0E-10	R22 ^{h)}	$\text{e} + \text{He} \rightarrow \text{He}^+ + 2\text{e}$	$2.5\text{E}-12T_e^{0.68}$ $\exp(-24.6/T_e)$
R5 ^{b)}	$\text{O}_2 + \text{O}^+ \rightarrow \text{O}_2^+ + \text{O}$	2.0E-11	R23 ^{h)}	$\text{e} + \text{He}_2^+ \rightarrow \text{He}^+ + \text{He}$	$5.386\text{E}-7T_e^{0.5}$
R6 ^{a)}	$\text{e} + \text{O}_2 \rightarrow \text{O}_2(^1\Delta_g) + \text{e}$	1.7E-9 $\exp(-3.1/T_e)$	R24 ^{h)k)}	$\text{He}^+ + 2\text{He} \rightarrow \text{He}_2^+ + \text{He}$	1.3E-33
R7 ^{a)}	$\text{O}^- + \text{O}_2(^1\Delta_g) \rightarrow \text{O}_3 + \text{e}$	3.0E-10	R25 ^{h)k)}	$\text{He}^+ + 2\text{He} \rightarrow \text{He}_2^+ + \text{He}$	1.3E-31
R8 ^{a)}	$\text{O}^- + \text{O}_2(^1\Delta_g) \rightarrow \text{O}_2^- + \text{O}$	1.0E-10	R26 ^{j)}	$\text{He}_2^+ + \text{He}_2^* \rightarrow \text{He}_2^+ + 2\text{He} + \text{e}$	1.5e-9
R9 ^{a)}	$\text{e} + \text{O}_2 \rightarrow \text{O} + \text{O}(^1\text{D}) + \text{e}$	5.0E-8 $\exp(-8.4/T_e)$	R27 ⁱ⁾	$\text{O}(^1\text{D}) + \text{O}_2 \rightarrow \text{O} + \text{O}_2$	3.0e-11
R10 ^{a)}	$\text{e} + \text{O} \rightarrow \text{O}(^1\text{D}) + \text{e}$	4.2E-9 $\exp(-2.25/T_e)$	R28 ^{d)}	$\text{O}(^1\text{D}) + \text{He} \rightarrow \text{O} + \text{He}$	1.0e-13
R11 ^{c)}	$\text{O}_2(^1\Sigma_g^+) + \text{O}_3 \rightarrow \text{O} + 2\text{O}_2$	1.5E-11	R29 ^{e)}	$\text{O}_2(^1\Sigma_g^+) + \text{O} \rightarrow \text{O}_2(^1\Delta_g) + \text{O}$	3.0e-12
R12 ^{a)}	$\text{O}^* + \text{O}_2 \rightarrow \text{O} + \text{O}_2(^1\Sigma_g^+)$	2.0E-11	R30 ⁱ⁾	$\text{e} + \text{O}_3 \rightarrow \text{O}^- + \text{O}_2$	$9.3\text{E}-10T_e^{-0.62}$
R13 ^{d)}	$\text{e} + \text{O}_2 \rightarrow \text{O} + \text{O} + \text{e}$	4.2E-9 $\exp(-5.6/T_e)$	R31 ⁱ⁾	$\text{e} + \text{O}_3 \rightarrow \text{O} + \text{O}_2^-$	2.0e-10
R14 ^{e)}	$\text{O}_2(^1\Delta_g) + \text{O}_3 \rightarrow 2\text{O}_2 + \text{O}^*$	1.0E-11	R32 ⁱ⁾	$\text{O}_3^- + \text{O}_2^+ \rightarrow 2\text{O} + \text{O}_3$	$1.01\text{E}-7(300/T)^{0.5}$
R15 ^{d)}	$\text{e} + \text{O} \rightarrow \text{O}^+ + 2\text{e}$	$9.0\text{E}-9T_e^{0.7}$ $\exp(-13.6/T_e)$	R33 ⁱ⁾	$\text{e} + \text{O}_3 \rightarrow \text{O} + \text{O}_2 + \text{e}$	$1\text{E}-8(300/T)^{0.5}$
R16 ^{e)}	$\text{O}^- + \text{O}_3 \rightarrow \text{O}_3^- + \text{O}$	5.3E-10	R34 ^{d)}	$\text{He}^+ + \text{O}_2 \rightarrow \text{O}^+ + \text{O} + \text{He}$	$1.07\text{E}-9(T/300)^{0.5}$
R17 ^{e)}	$\text{O}_3^- + \text{O} \rightarrow 2\text{O}_2 + \text{e}$	3.0E-10	R35 ^{e)}	$\text{O}_2^- + \text{M} \rightarrow \text{O}_2 + \text{M} + \text{e}$	$2.7\text{E}-10(T/300)^{0.5}$ $\exp(-5\,590/T)$
R18 ^{e)}	$\text{O}_3^- + \text{O} \rightarrow \text{O}_2^- + \text{O}_2$	3.2E-10			

^{a)}Ref. [11]; ^{b)}Ref. [15]; ^{c)}Ref. [16]; ^{d)}Ref. [17]; ^{e)}Ref. [18]; ^{f)}Ref. [19]; ^{g)}Ref. [20]; ^{h)}Ref. [21]; ⁱ⁾Ref. [22]; ^{j)}Ref. [23]; ^{k)}Rate constants are in $\text{cm}^6 \cdot \text{s}^{-1}$.

dominant reactions of those typically chosen in other models such as fluid and particle-in-cell models, it would help them to reduce their computation time. For He/O₂ mixture, 35 key reactions of 98 reactions used in our model are selected by means of analyzing the reaction rates for each species and picking up the dominant reactions, as listed in Table 1. Figure 8 shows the comparisons of the electron and the atomic oxygen density obtained from calculations with all 98 reactions and selected 35 reactions. The model with the selected 35 key reactions can reproduce the quite close results for electron and atomic oxygen densities to those obtained from the model with

98 reactions for wide ranges of the input power, as shown in Figure 8(a) and (b).

Conclusion

We have developed a global model of He/O₂ atmospheric pressure discharges widely used in the biomedical applications such as sterilization, coagulation, and wound healing to identify the dominant reactions and the main species. Similar trend to an experimental measurement of the atomic oxygen density was observed through the global

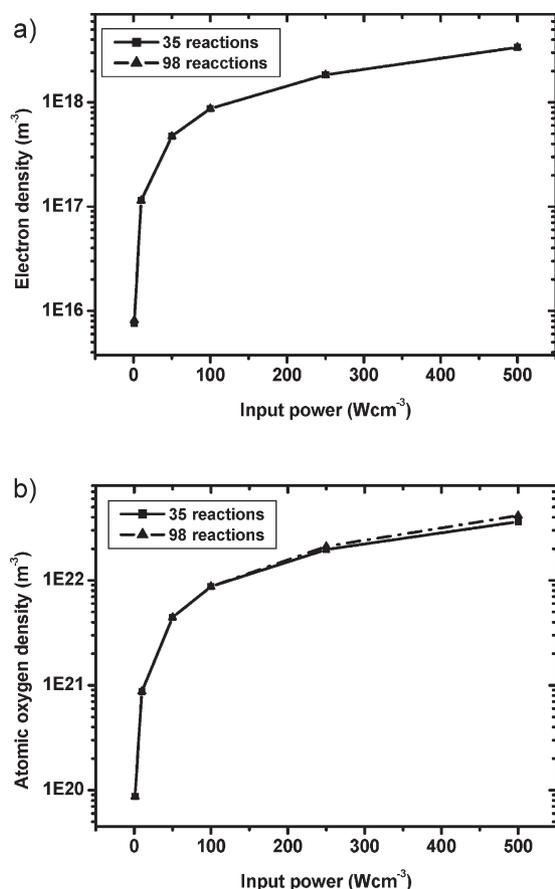


Figure 8. The comparisons of (a) the electron density and (b) the atomic oxygen density obtained from models to consider 35 key reactions and 98 reactions.

model while varying the concentration of O_2 . The maximum atomic oxygen density appeared at an admixture of 0.4% of O_2 when the input power was $330 \text{ W} \cdot \text{cm}^{-3}$. With increase in the concentration of O_2 , the dissociation of O_2 increased to produce the atomic oxygen, and the recombinations of the atomic oxygen with themselves or oxygen molecules and the thermal wall loss became the dominant loss processes for the atomic oxygen. With decrease in the input power, the maximum density of the atomic oxygen was observed at lower concentration of O_2 . The 35 key reactions of He/O_2 were selected through the analysis of reaction rates for each species and they reproduced almost same results as those obtained from the calculations to take into account 98 reactions. The global model could be used to identify the dominant reactions and would be helpful to reduce the computational time for simulations of biomedical atmospheric pressure discharges.

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- [1] M. Laroussi, *Plasma Process. Polym.* **2005**, *2*, 391.
- [2] S. U. Kalghatgi, G. Fridman, M. Cooper, G. Nagaraj, M. Peddinghaus, M. Balasubramanian, V. N. Vasilets, A. F. Gutsol, A. Fridman, G. Friedman, *IEEE Trans. Plasma Sci.* **2007**, *35*, 1559.
- [3] G. Fridman, G. Friedman, A. Gutsol, A. B. Shekhter, V. N. Vasilets, A. Fridman, *Plasma Process. Polym.* **2008**, *5*, 503.
- [4] G. C. Kim, G. J. Kim, S. R. Park, S. M. Jeon, H. J. Seo, F. Iza, J. K. Lee, *J. Phys. D: Appl. Phys.* **2009**, *42*, 032005; *Europhys. News* **2009**, *40*, 14.
- [5] M. Moravej, X. Yang, R. F. Hicks, J. Penelon, S. E. Babayan, *J. Appl. Phys.* **2006**, *99*, 093305.
- [6] N. Knake, K. Niemi, S. Reuter, V. S. Gathen, J. Winter, *Appl. Phys. Lett.* **2008**, *93*, 131503.
- [7] E. Stoffels, I. E. Kieft, R. E. J. Sladek, *J. Phys. D: Appl. Phys.* **2003**, *36*, 2908.
- [8] J. Choi, F. Iza, H. J. Do, J. K. Lee, M. H. Cho, *Plasma Sources Sci. Technol.* **2009**, *18*, 025029.
- [9] X. Deng, J. Shi, M. G. Kong, *IEEE Trans. Plasma Sci.* **2006**, *34*, 1310.
- [10] S. J. Kim, T. H. Chung, S. H. Bae, S. H. Leem, *Appl. Phys. Lett.* **2009**, *94*, 141502.
- [11] M. A. Lieberman, A. J. Lichtenberg, *Principle of Plasma Discharges and Materials Processing*, Wiley, New York 2005.
- [12] G. Y. Park, H. W. Lee, G. C. Kim, J. K. Lee, *Plasma Process. Polym.* **2008**, *5*, 569.
- [13] S. J. Kim, M. A. Lieberman, A. J. Lichtenberg, J. T. Gudmundsson, *J. Vac. Sci. Technol., A* **2006**, *24*, 2025.
- [14] H. J. Lee, J. K. Lee, *Jpn. J. Appl. Phys.* **1996**, *35*, 6252.
- [15] A. B. Rakshit, H. M. P. Stock, D. P. Wareing, N. D. Twiddy, *J. Phys. B: At. Mol. Phys.* **1978**, *11*, 4237.
- [16] D. L. Baulch, R. A. Cox, P. J. Crutzen, R. F. Hampson, Jr., J. A. Kerr, J. Troe, R. T. Watson, *J. Phys. Chem. Ref. Data* **1982**, *11*, 327.
- [17] D. S. Stafford, M. J. Kushner, *J. Appl. Phys.* **2004**, *96*, 2451.
- [18] C. Soria, F. Pontiga, A. Castellanos, *Plasma Sources Sci. Technol.* **2004**, *13*, 95.
- [19] W. Lindinger, A. L. schmeltkopf, F. C. Fehsenfeld, *J. Chem. Phys.* **1974**, *61*, 2890.
- [20] J. Y. Jeong, J. Park, I. Henins, S. E. Babayan, V. J. Tu, G. S. Selwyn, G. Ding, R. F. Hicks, *J. Phys. Chem. A* **2000**, *104*, 8027.
- [21] S. Rauf, M. J. Kushner, *J. Appl. Phys.* **1999**, *85*, 3460.
- [22] J. T. Gudmundsson, I. G. Kouznetsov, K. K. Patel, M. A. Lieberman, *J. Phys. D: Appl. Phys.* **2001**, *34*, 1100.
- [23] R. Deloche, P. Monchicourt, M. Cheret, F. Lambert, *Phys. Rev. A* **1976**, *13*, 1140.